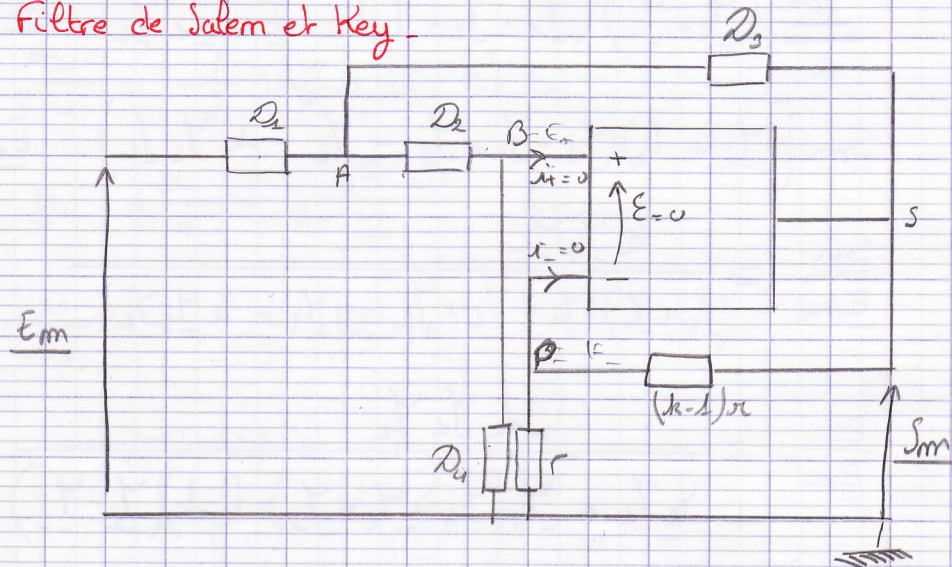


## DM24 - Filtre actif et satellite -

### I - Filtre de Salem et Key



1) amplificateur opérationnel idéal:  $i_+ = i_- = 0$   
 régime linéaire  $\left\{ \begin{array}{l} \text{le gain de l'amplificateur tend vers l'infini} \\ E = E_+ - E_- = 0 \end{array} \right. \Rightarrow \underline{V_p = V_o} \quad (1)$

#### 2) Théorème de Millman en A

$$\underline{V_A} = \frac{E_{in} Y_2 + S_{in} Y_3 + V_o Y_4}{Y_2 + Y_3 + Y_4} \quad (2)$$

#### Théorème de Millman en B

$$\underline{V_B} = \frac{\underline{V_A} Y_2 + \underline{V_o} Y_4 + 0}{Y_2 + Y_4}$$

$$\underline{V_A} = \frac{V_o (Y_2 + Y_4)}{Y_2} \quad (3)$$

Pont diviseur de tension:  $\underline{V_p} = \frac{r}{(R-1)r + r} S_{in}$

$$\underline{V_p} = \frac{1}{(R-1)+1} S_{in}$$

$$\underline{V_p} = \frac{S}{R} \quad (4)$$

(2) (1)  
 (3) (4) →

$$\underline{V}_a = \frac{1/2 (\underline{Y}_2 + \underline{Y}_4) \underline{S}_{mn}}{\underline{Y}_e} = \frac{\underline{E}_{mn} \underline{Y}_2 + 1/2 \underline{S}_{mn} \underline{Y}_2 + \underline{Y}_3 \underline{Y}_2}{\underline{Y}_2 + \underline{Y}_e + \underline{Y}_3}$$

$$\frac{\underline{S}_{mn}}{R} (\underline{Y}_2 + \underline{Y}_4) (\underline{Y}_2 + \underline{Y}_e + \underline{Y}_3) = \underline{E}_{mn} \underline{Y}_2 \underline{Y}_2 + \frac{\underline{S}_{mn}}{R} \underline{Y}_2^2 + \underline{S}_{mn} \underline{Y}_3 \underline{Y}_2$$

$$\underline{S}_{mn} \left[ (\underline{Y}_2 + \underline{Y}_4) (\underline{Y}_2 + \underline{Y}_e + \underline{Y}_3 - \underline{Y}_2) - \underline{Y}_2^2 - k \underline{Y}_3 \underline{Y}_2 \right] = \underline{E}_{mn} k \underline{Y}_2 \underline{Y}_2$$

$$\frac{\underline{S}_{mn}}{\underline{E}_{mn}} = \frac{k \underline{Y}_2 \underline{Y}_2}{(\underline{Y}_2 + \underline{Y}_4) (\underline{Y}_2 + \underline{Y}_e + \underline{Y}_3 - \underline{Y}_2) - \underline{Y}_2^2 - k \underline{Y}_3 \underline{Y}_2}$$

$$\frac{\underline{S}_{mn}}{\underline{E}_{mn}} = \frac{k \underline{Y}_2 \underline{Y}_2}{\underline{Y}_2 \underline{Y}_2 + \underline{Y}_4 (\underline{Y}_2 + \underline{Y}_e + \underline{Y}_3) + (1-k) \underline{Y}_2 \underline{Y}_3}$$

$$H = \frac{R \cdot 1/R \cdot C\omega}{j \frac{C\omega}{R} + \left( \frac{1}{R} + j C\omega \right) \left( \frac{1}{R} + j C\omega \right) + j \frac{C\omega}{R} (1-k)}$$

$$H = \frac{k R C\omega}{j R C\omega + (1 + j R C\omega) (1 + j R C\omega) + j R C\omega (1-k)}$$

$$H = \frac{k j R C\omega}{j R C\omega + 1 + 2 j R C\omega + (j R C\omega)^2 + j R C\omega (1-k)}$$

$$H = \frac{k j R C\omega}{1 + j R C\omega (5-k) + (j R C\omega)^2}$$

$$H = \frac{j \frac{R C\omega}{2}}{1 + j R C\omega \frac{(5-k)}{2} + \frac{(j R C\omega)^2}{2}}$$

Forme canonique associée :

$$H = \frac{H_0 j \frac{\omega}{\omega_0}}{1 + j \frac{\omega}{\omega_0} + \left( \frac{\omega}{\omega_0} \right)^2}$$

Identification:  $\alpha = \frac{\omega}{\omega_0}$

$$\begin{cases} (j\alpha)^2 = \frac{1}{2} (jRC\omega)^2 & (1) \\ j\frac{\alpha}{Q} = \frac{1}{2} jRC\omega (5-k) & (2) \\ \underline{H_0} \cdot j\frac{\alpha}{Q} = j\frac{kRC\omega}{2} & (3) \end{cases}$$

$$(1) \left(\frac{\omega}{\omega_0}\right)^2 = \frac{1}{2} (RC\omega)^2$$

$$\Leftrightarrow \omega_0^2 = \frac{2}{(RC)^2}$$

$$\Leftrightarrow \boxed{\omega_0 = \frac{\sqrt{2}}{RC}}$$

$$(2) \frac{\omega}{\omega_0 Q} = \frac{1}{2} (RC\omega)(5-k)$$

$$\boxed{Q = \frac{2}{\omega_0 RC(5-k)} = \frac{\sqrt{2}}{5-k}}$$

$$(3) \frac{H_0 \cdot \omega}{-j\omega_0 Q} = j\frac{kRC\omega}{2} \Leftrightarrow \underline{H_0} = \frac{Q\omega_0 k RC}{2}$$

$$\Leftrightarrow \boxed{H_0 = \frac{k}{5-k}}$$